

Multiscale models of metal plasticity

Lecture IV: Kinetics and work hardening

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Sixth Summer School in Analysis and
Applied Mathematics

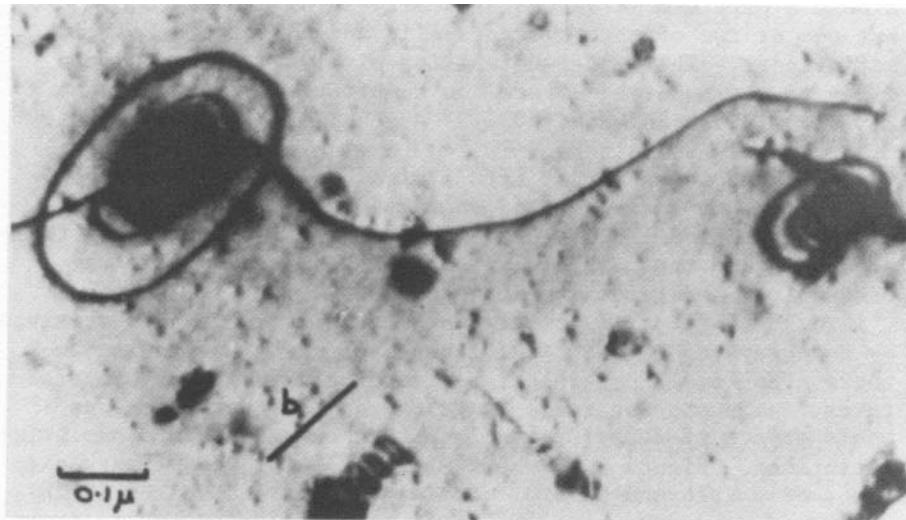
Rome, June 20-24, 2011



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Outline of Lecture #4

- Beyond energy: Kinetics
- Experimental observations, dislocation mobility
- The forest hardening model
- Energy-dissipation functionals
- Phase-field models

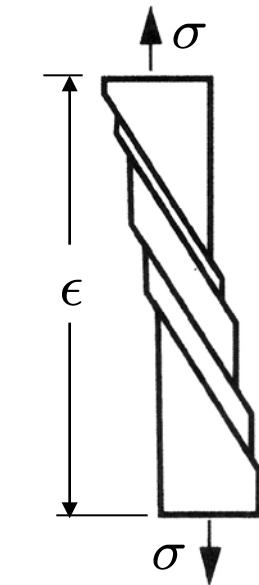


(Humphreys and Hirsch, 1970)

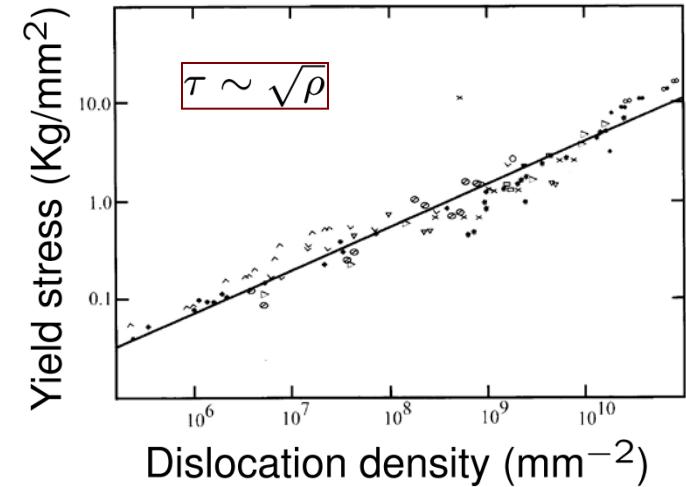
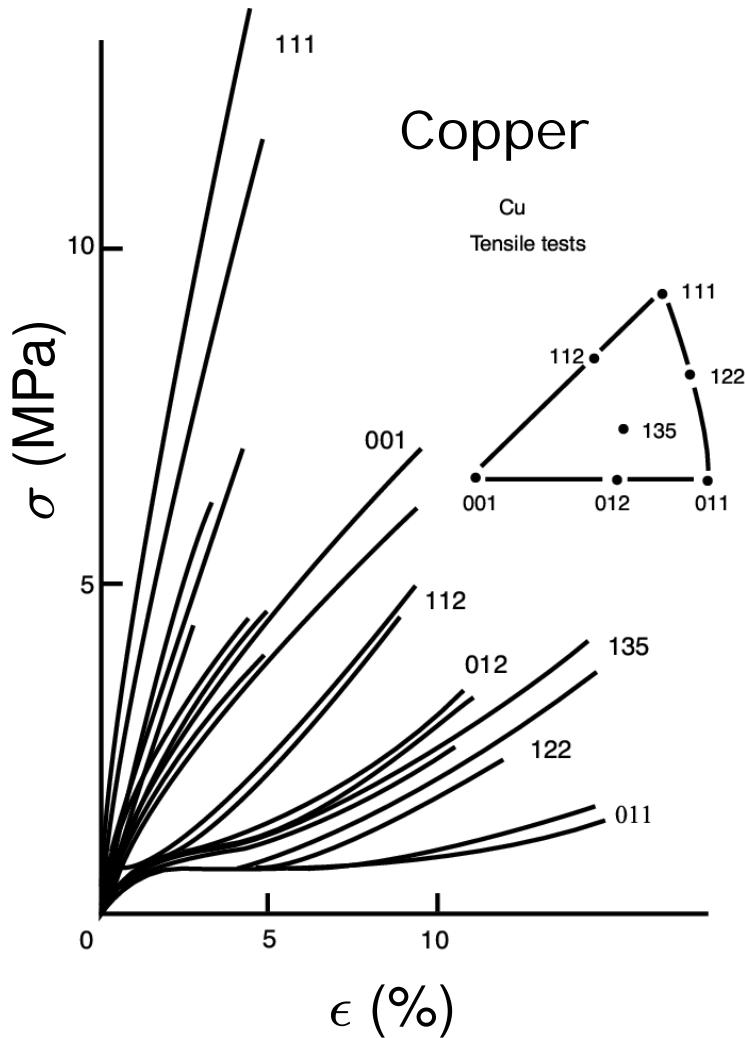


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Crystal plasticity – Macroscopic behavior



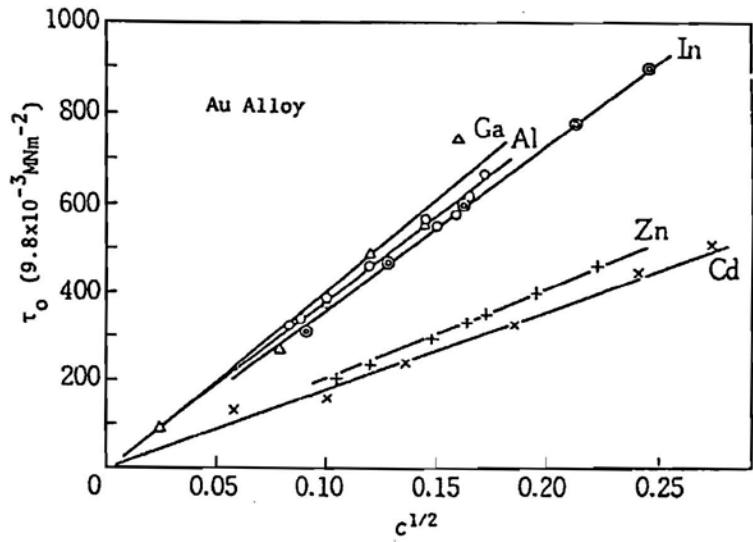
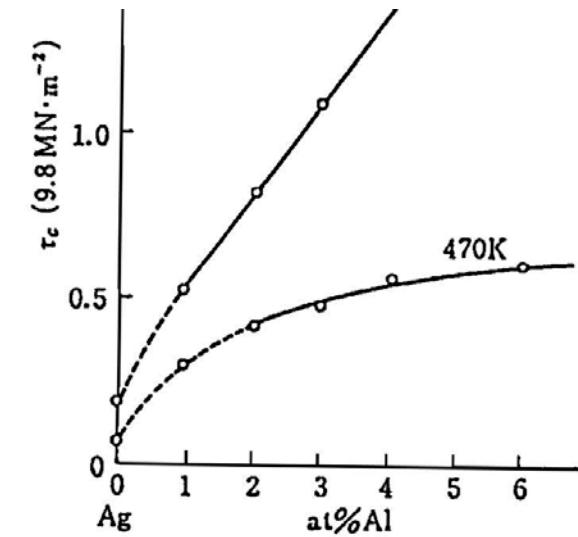
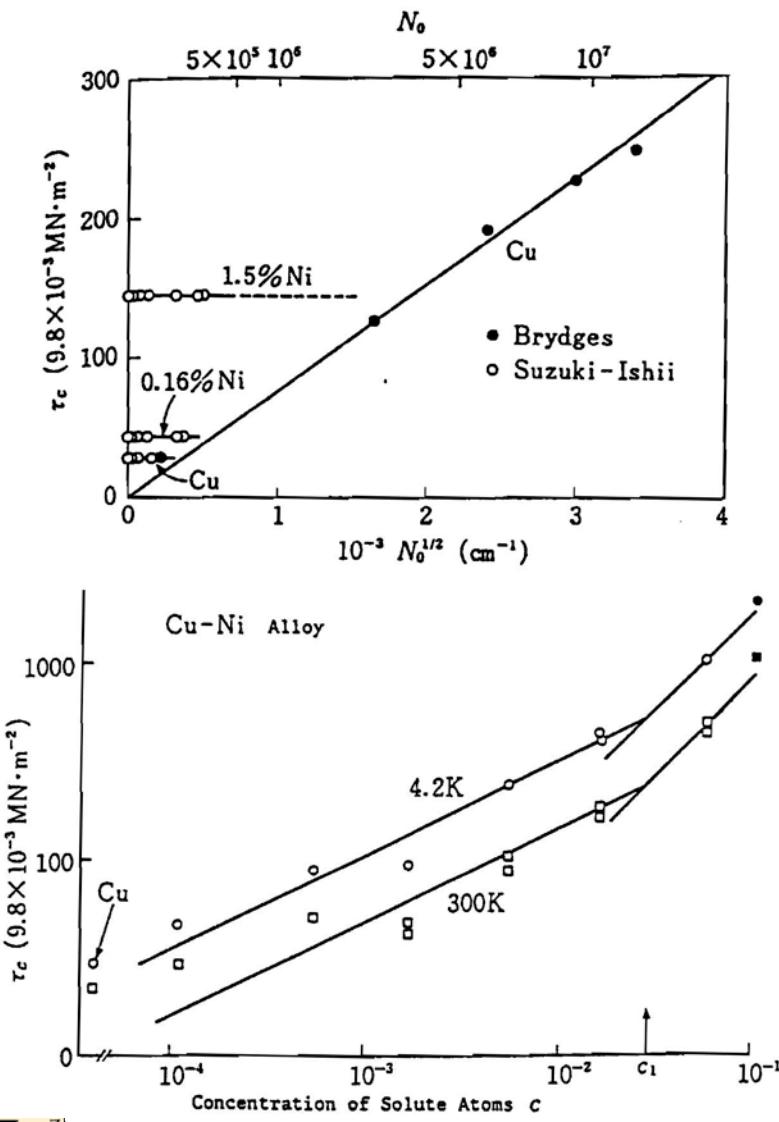
Uniaxial
tension test



Taylor scaling
(SJ Basinski and ZS Basinski,
Dislocations in Solids,
FRN Nabarro (ed.)
North-Holland, 1979.)

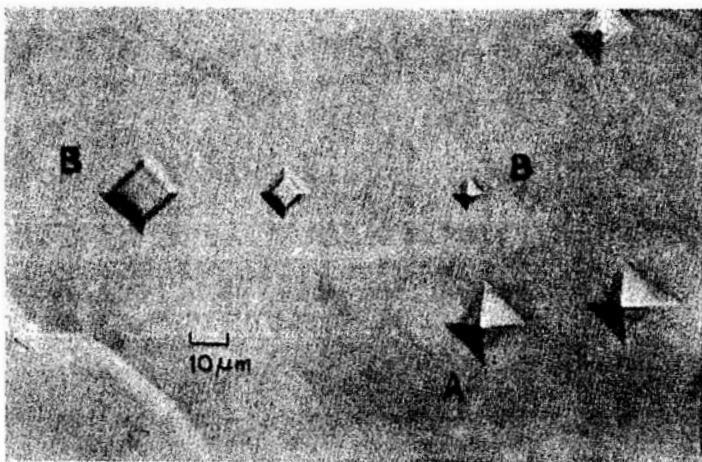
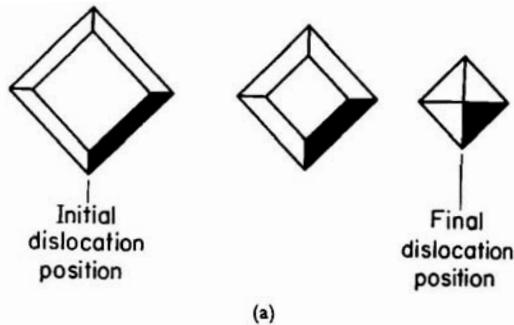


Hardening and obstacle density

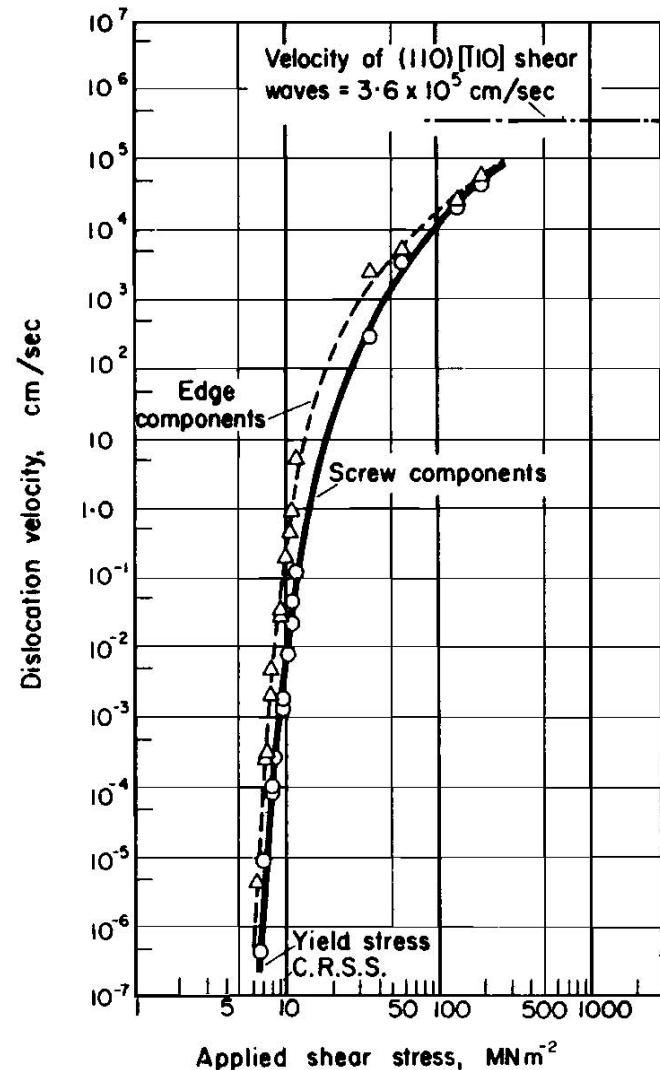


T. Suzuki, S. Takeuchi and H. Yoshinaga,
Dislocation Dynamics and Plasticity, Springer-Verlag, 1985.

Dislocation velocity



Etch pits on a LiF crystal

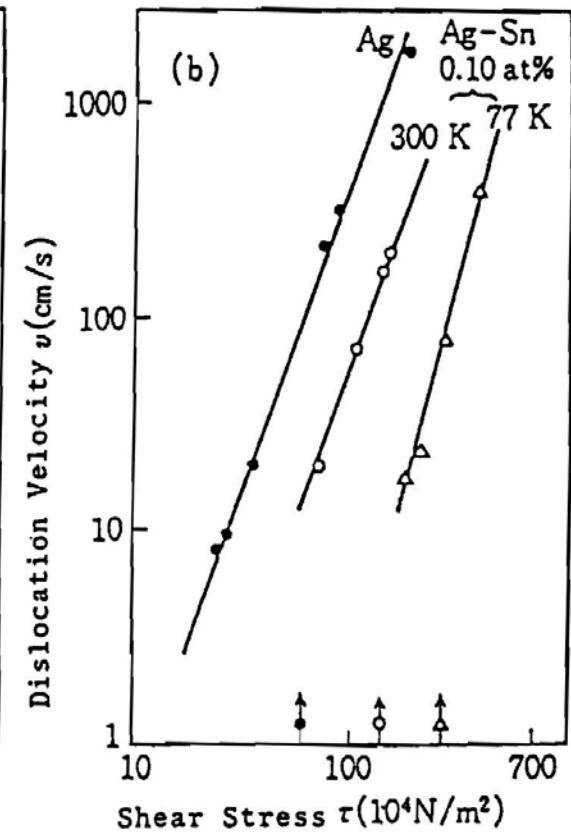
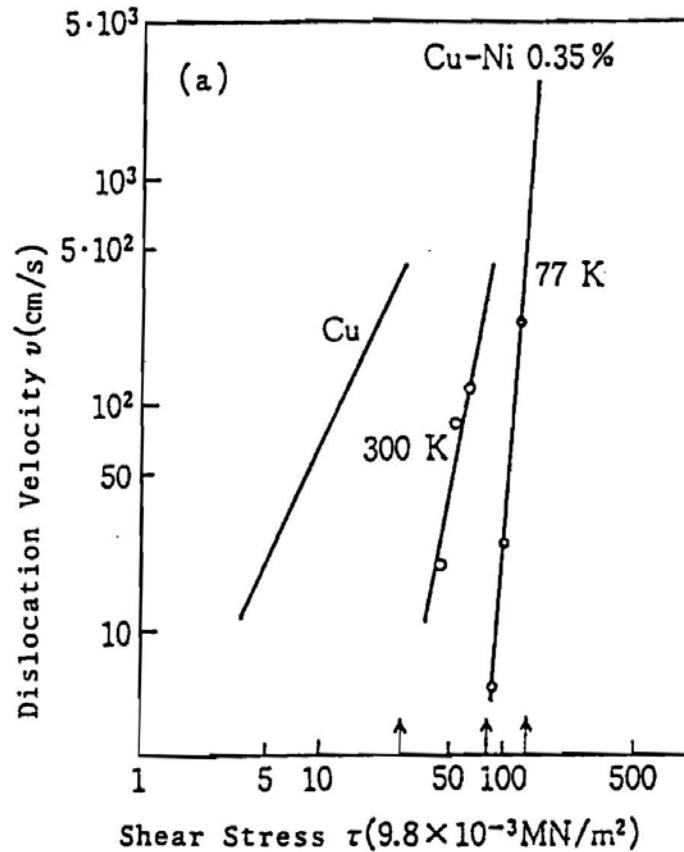
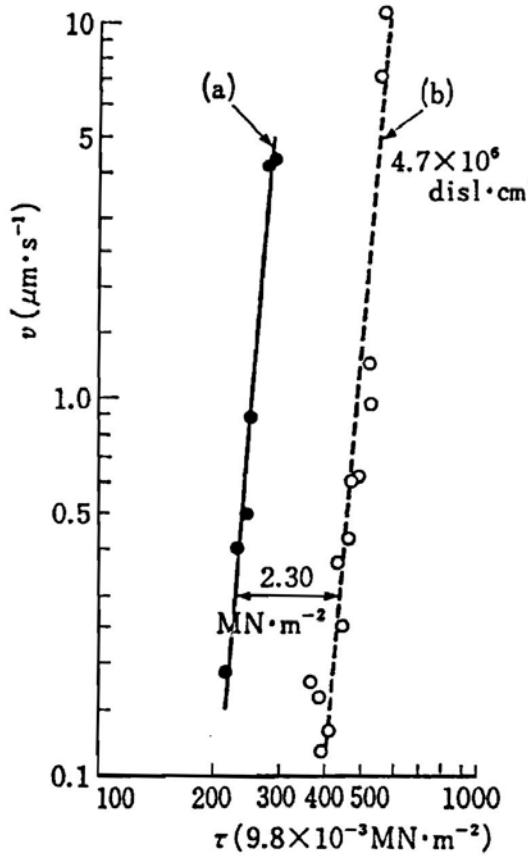


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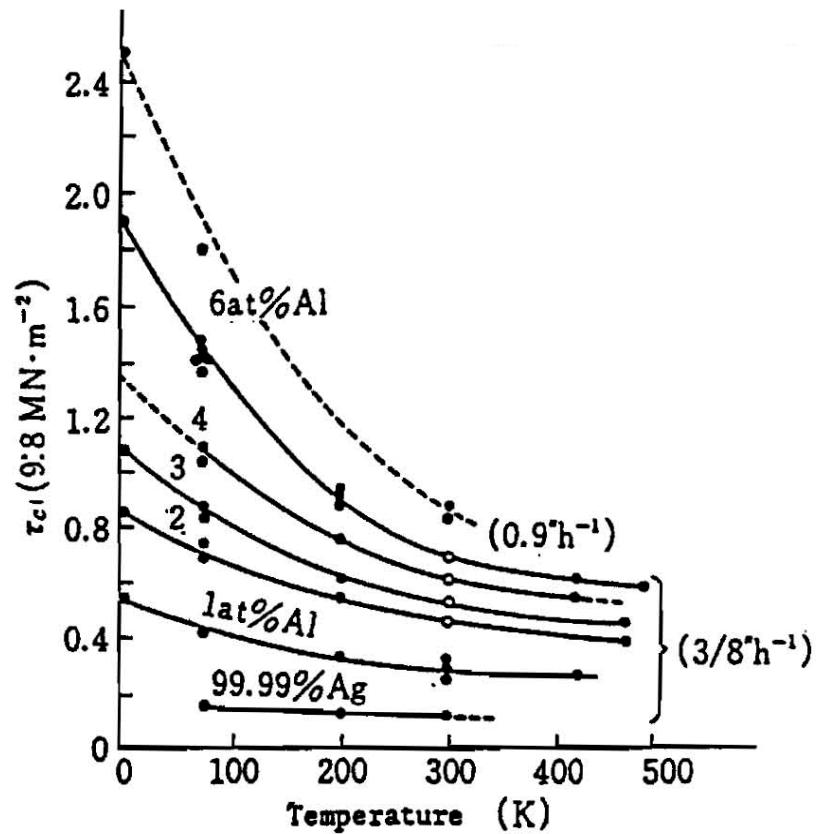
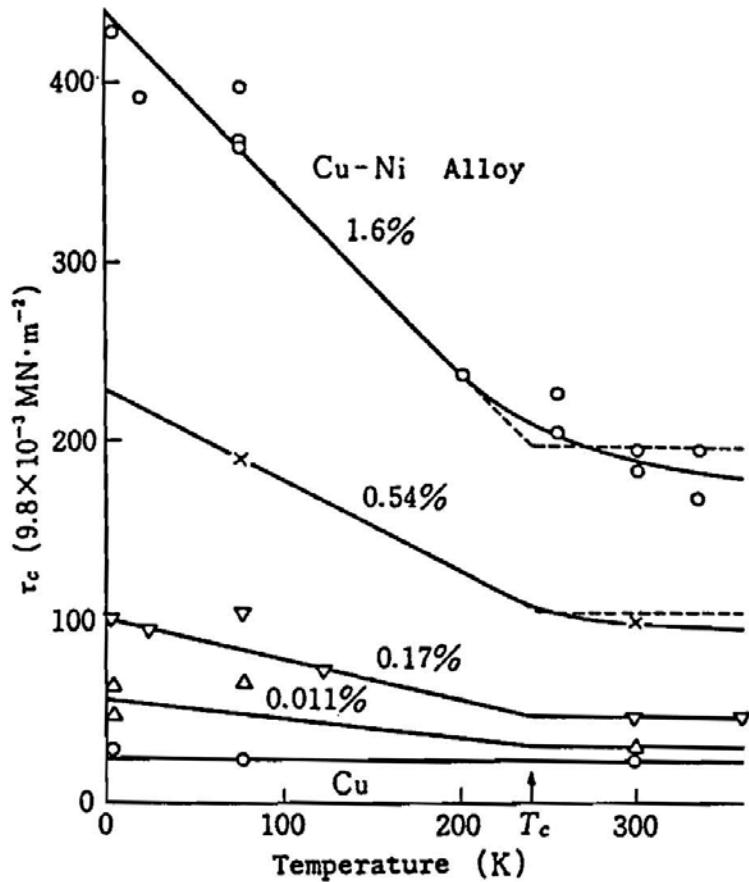
Dislocation velocity



T. Suzuki, S. Takeuchi and H. Yoshinaga,
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Thermal softening

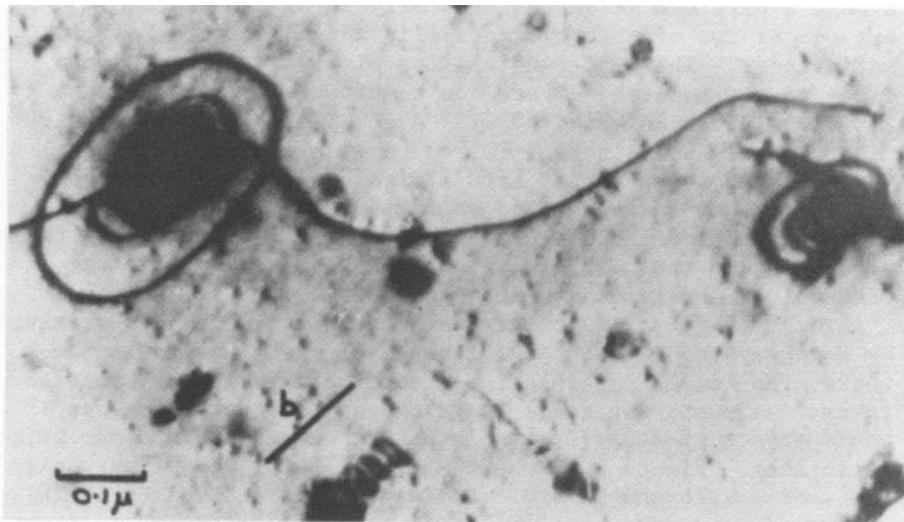


T. Suzuki, S. Takeuchi and H. Yoshinaga,
Dislocation Dynamics and Plasticity, Springer-Verlag, 1985.

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Outline of Lecture #4

- Dislocation motion is governed by kinetics
- Dislocations react with each other irreversibly
- Energy-minimization is not enough to describe dislocation dynamics, hardening
- Need kinetics, time-dependent problems!

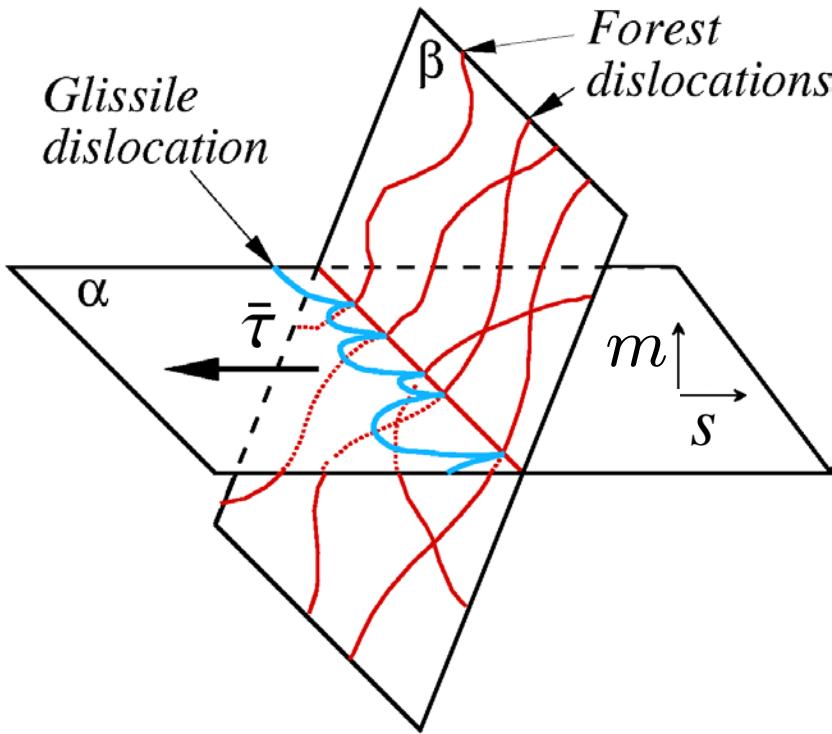


(Humphreys and Hirsch, 1970)

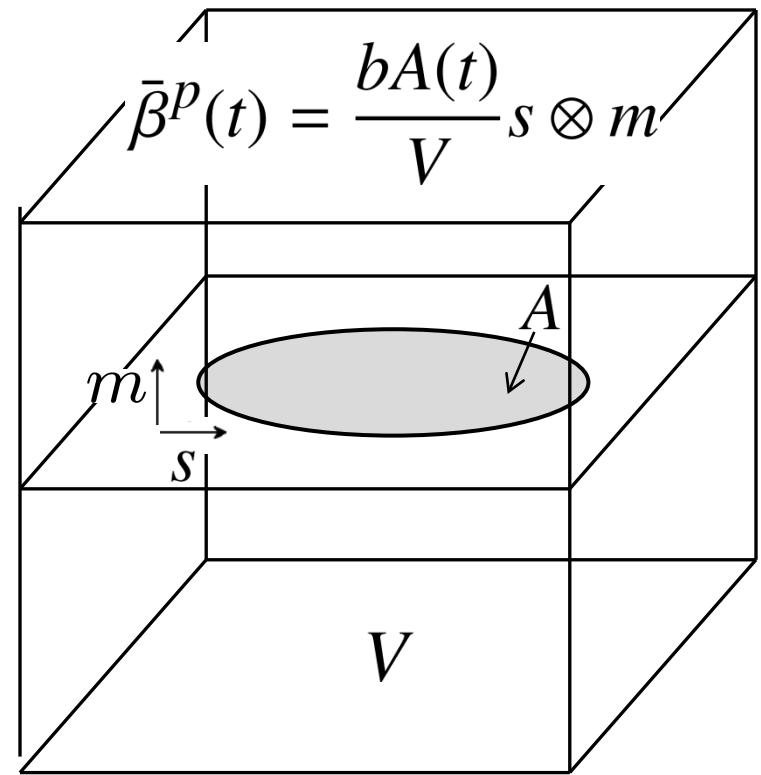


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The forest-hardening problem



Glissile dislocation moving
through forest dislocations



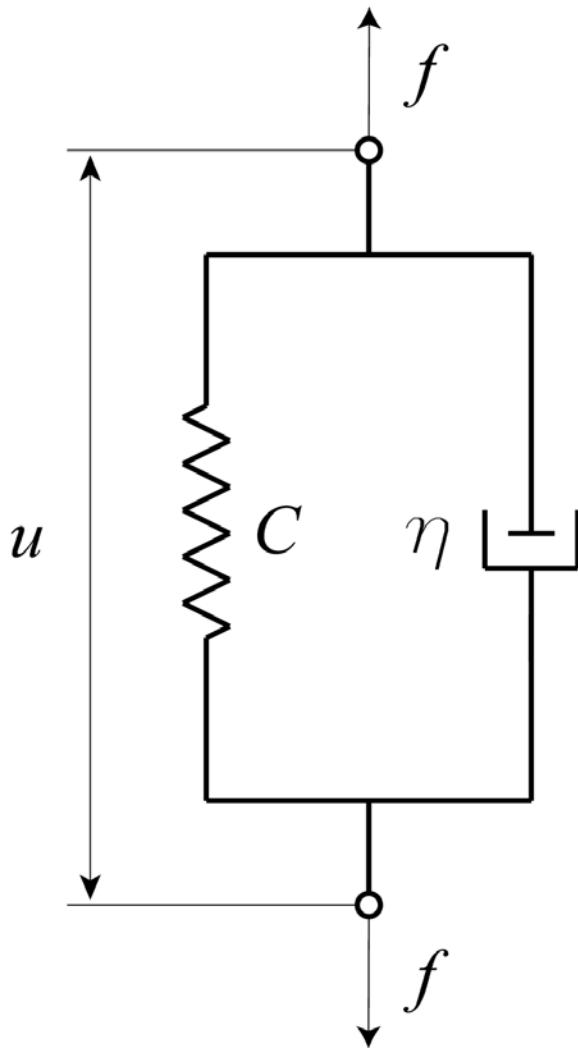
Micro-to-macro transition,
single slip

Given: $\bar{\tau}(t) = \bar{\sigma}_{ij}(t)s_i m_j$

determine: $\bar{\gamma}(t) = \frac{bA(t)}{V}$



Classical rate variational problems



- Kelvin solid IV problem:

$$\left. \begin{array}{l} \eta \dot{u}(t) + Cu(t) = f(t) \\ u(0) = u_0 \end{array} \right\}$$

- Potential energy:

$$E(t, u) = \frac{C}{2}u^2 - f(t)u$$

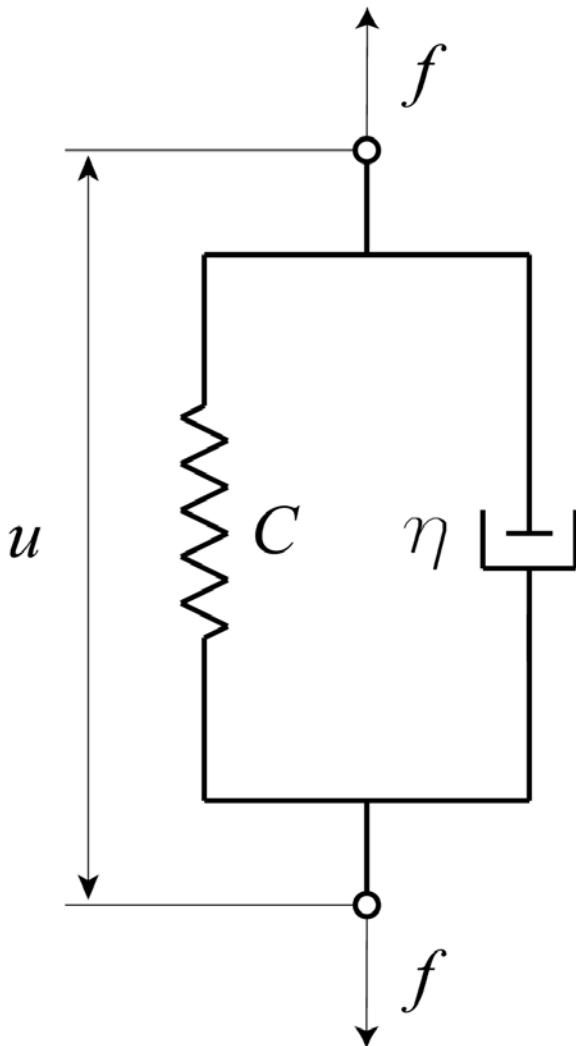
- Dissipation potential: $\Psi(v) = \frac{\eta}{2}v^2$

- Force equilibrium:

$$\partial\Psi(\dot{u}(t)) + DE(t, u(t)) = 0$$



Classical rate variational problems



- Rate potential:

$$G(t, u, v) \equiv \Psi(v) + DE(t, u) v$$

- Rate problem: Given $t, u,$

$$\min_v G(t, u, v)$$

- Euler-Lagrange equations:

$$\partial\Psi(v) + DE(t, u) = 0$$

- IV problem: For $t \in [0, T],$

$$\left. \begin{aligned} v(t) &\in \operatorname{argmin} G(t, u(t), \cdot) \\ \dot{u}(t) &= v(t), \quad u(0) = u_0 \end{aligned} \right\}$$



Forest hardening – External energy

- Energy of LE dislocated crystal, applied stress $\bar{\sigma}_{ij}$:

$$E(u) = \int_{\Omega \setminus J_u} \frac{1}{2} c_{ijkl} u_{i,j} u_{k,l} dx + \int_{\partial\Omega} \bar{\sigma}_{ij} n_j u_i d\mathcal{H}^2 = E^{\text{int}} + E^{\text{ext}}$$

- Potential of the externally applied stresses:

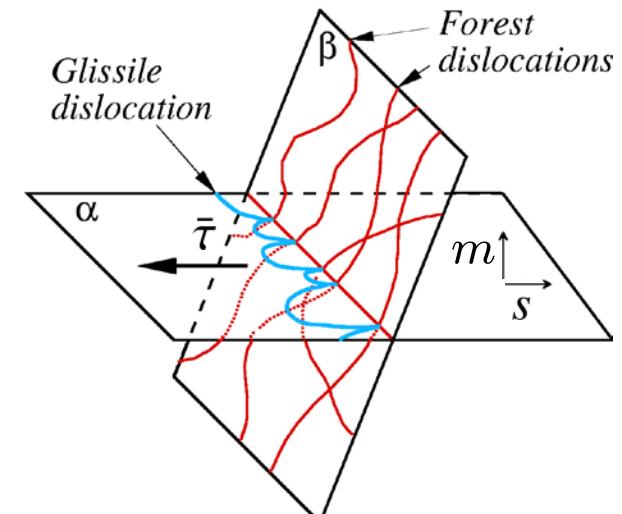
$$E^{\text{ext}} = \int_{\partial\Omega} \bar{\sigma}_{ij} u_i n_j d\mathcal{H}^2 = -\bar{\sigma}_{ij} \int_{J_u} [u_i] n_j d\mathcal{H}^2 = -V \bar{\sigma}_{ij} \bar{\beta}_{ij}^p$$

- Single slip on one single slip plane:

$$E^{\text{ext}} = -V \bar{\sigma}_{ij} \frac{A}{V} b_i m_j = -\bar{\tau} \bar{\gamma}, \quad \text{with:}$$

$$\bar{\tau} = \bar{\sigma}_{ij} s_i m_j \equiv \text{resolved shear stress}$$

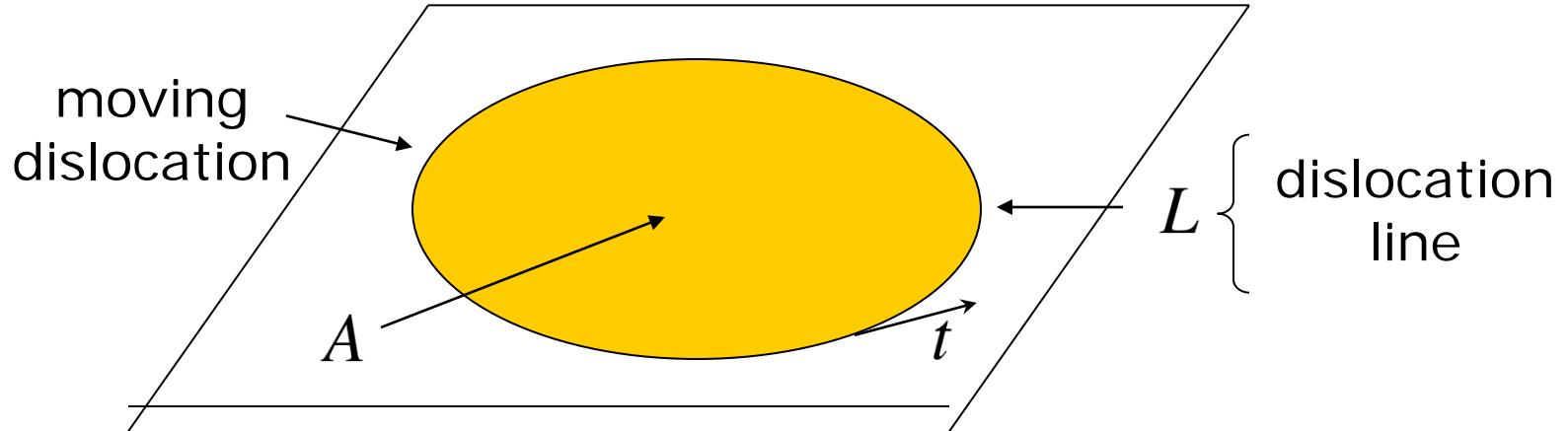
$$\bar{\gamma} = \frac{bA}{V} \equiv \text{macroscopic slip strain}$$



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Forest hardening – Stored energy

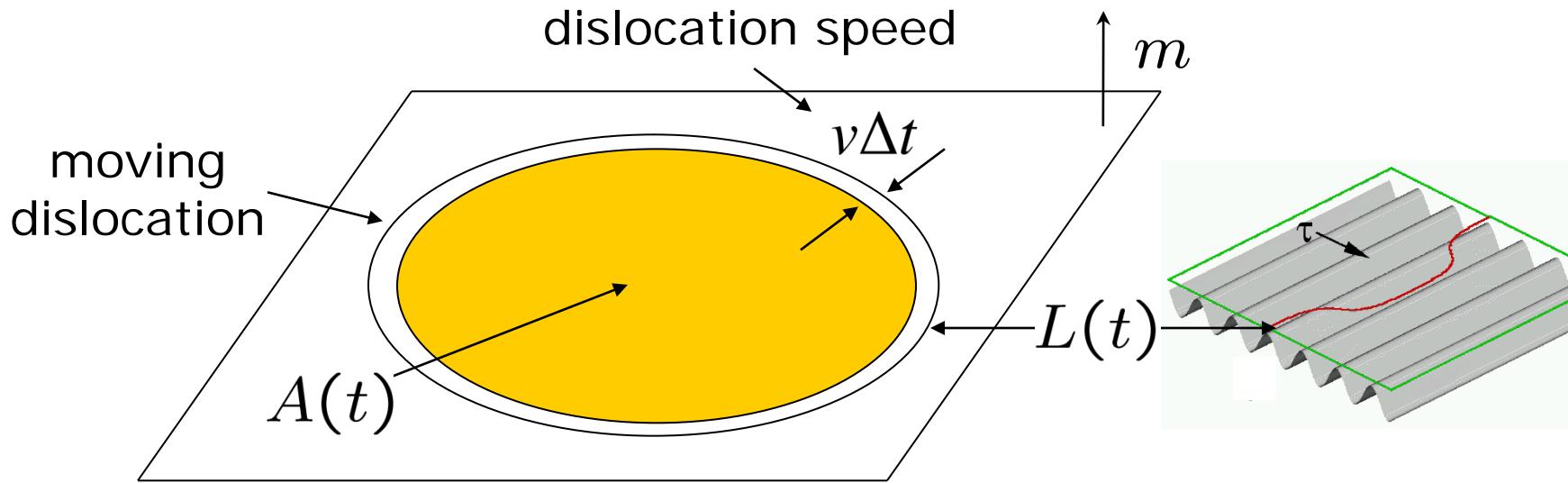


- Volterra dislocation density: $\alpha = d\beta^p = b \otimes t\mathcal{H}^1|_L$
- From Mura's formula, general representation: $E^{\text{int}}(\alpha)$
- Dilute limit, line-tension approximation:

$$E^{\text{int}}(\alpha) = \int_L \langle Kb, b \rangle d\mathcal{H}^1$$



Forest hardening – Lattice friction

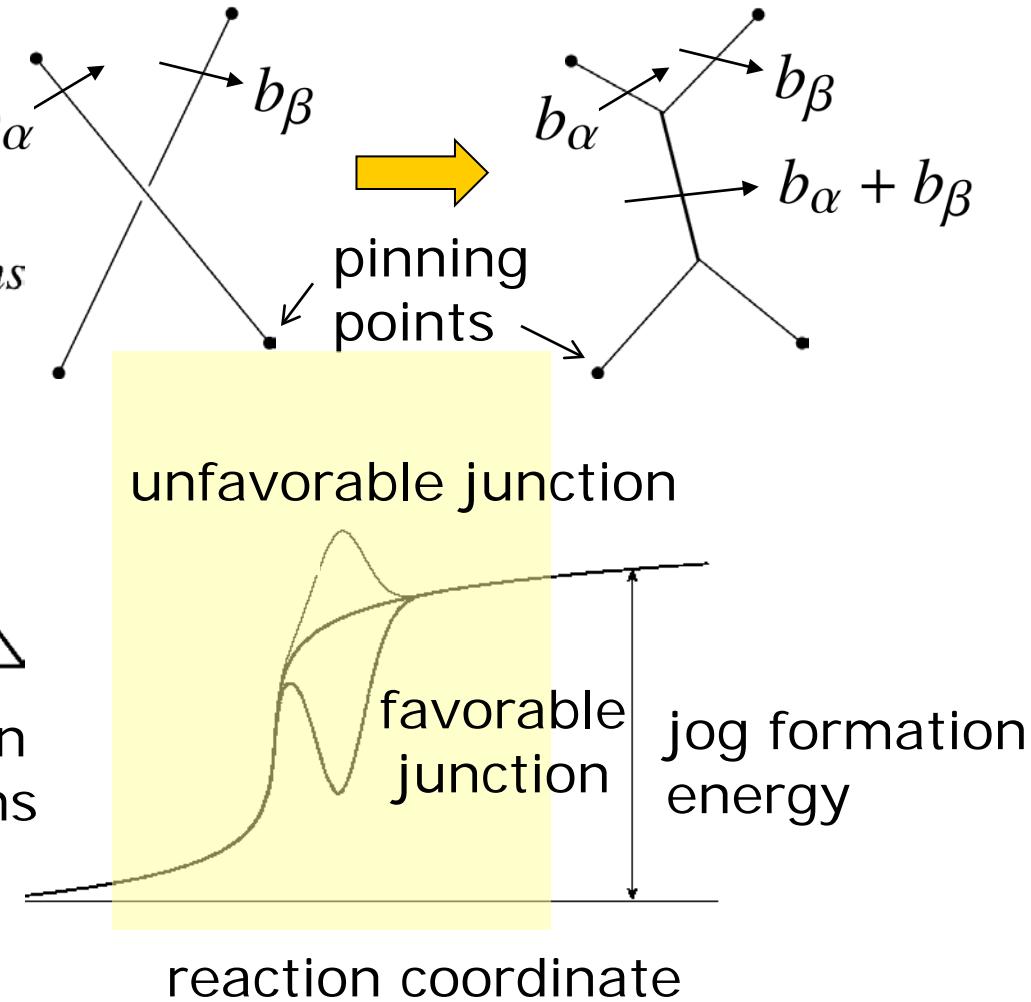
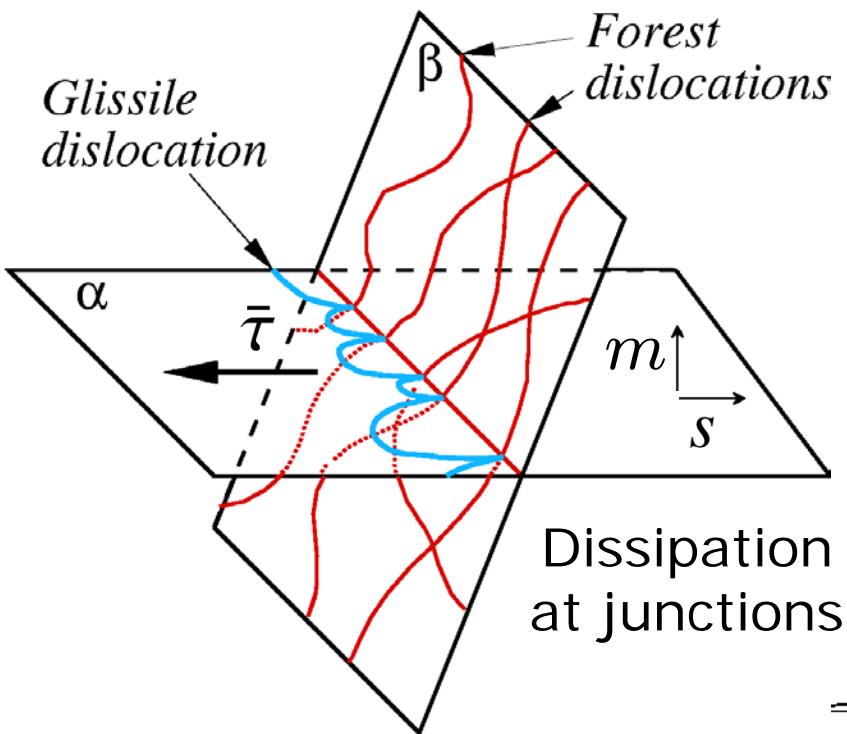


- Dislocation flux: $\forall \varphi \in C_0^1([0, T]), \forall f \in C_0(\Omega),$
$$\int_0^T \dot{\varphi} \left\{ \int [\![u]\!] \otimes m f d\mathcal{H}^2 \right\} dt = - \int_0^T \varphi \left\{ \int f d\underline{\mu(x)} \right\} dt$$
- Dislocation velocity: $\mu = -\alpha \times \underline{v}$ Peierls stress
 ↘ (lattice friction)
- Dissipation potential: $\Psi^{\text{lat}} = \int_L \tau_c |v| d\mathcal{H}^1$

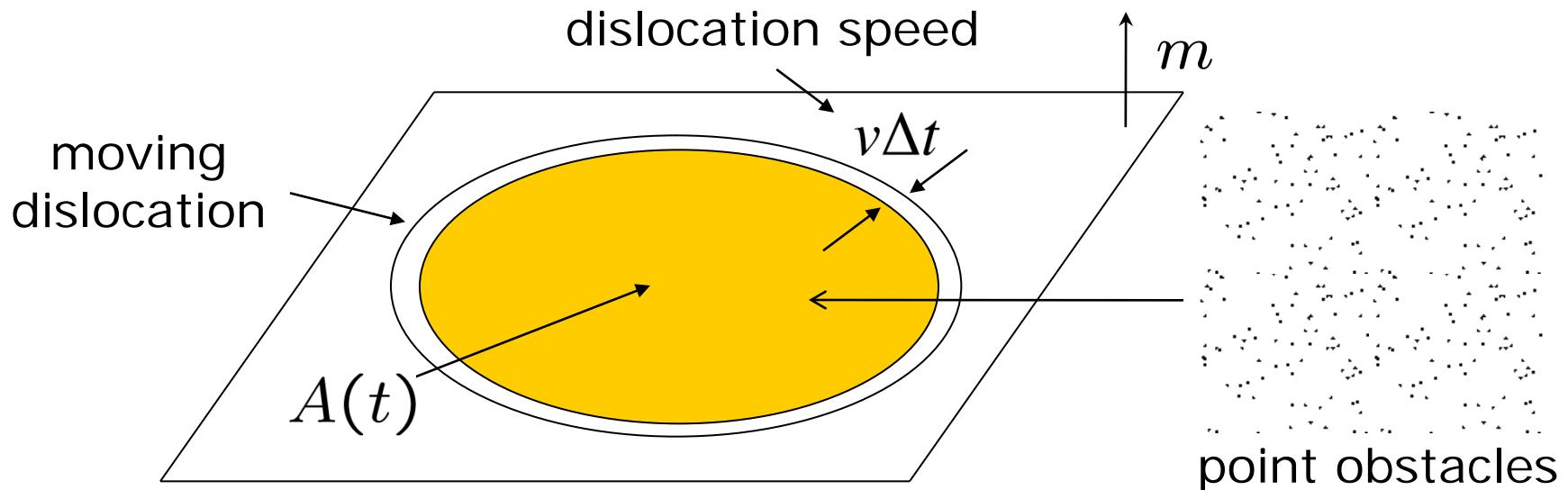


Forest hardening – Dissipation at obstacles

- Junctions, jogs:



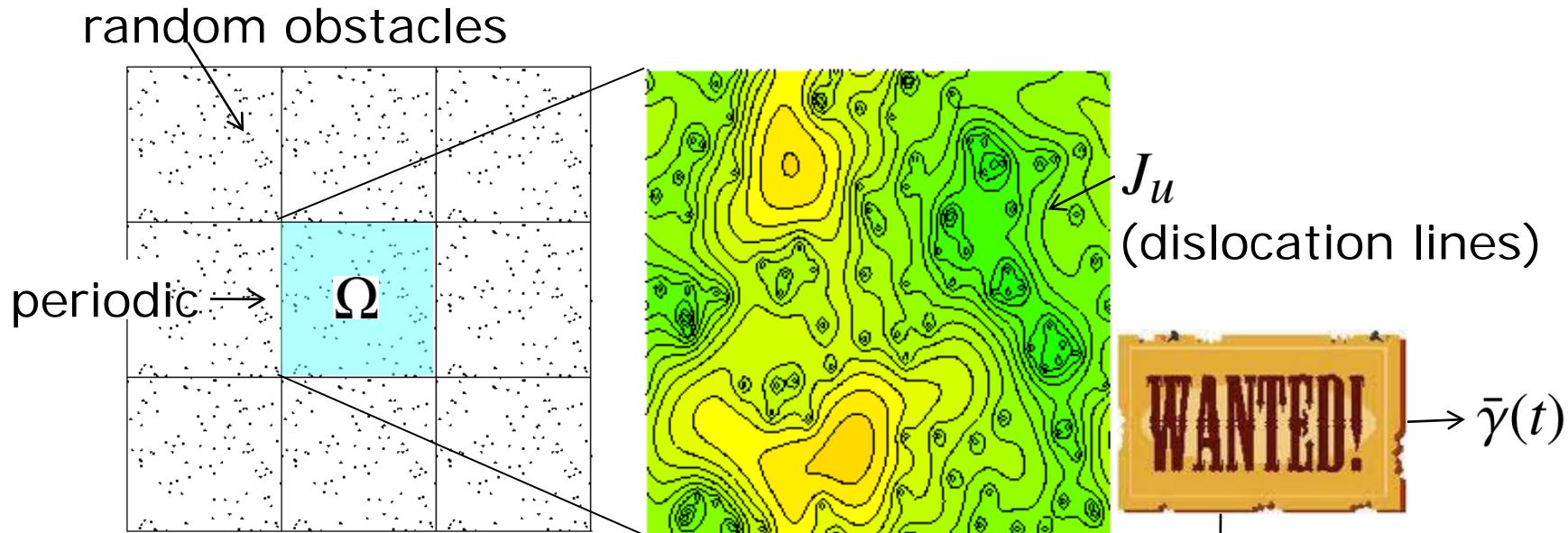
Forest hardening – Point obstacles



- Dislocation flux: $\forall \varphi \in C_0^1([0, T]), \forall f \in C_0(\Omega),$
$$\int_0^T \dot{\varphi} \left\{ \int [\![u]\!] \otimes m f d\mathcal{H}^2 \right\} dt = - \int_0^T \varphi \left\{ \int f d\underline{\mu(x)} \right\} dt$$
- Dislocation velocity: $\mu = -\alpha \times \underline{v}$
- Dissipation potential: $\Psi^{\text{obs}} = \sum_{\text{obstacles}} f_c |v|$



Forest hardening – Summary



- Find: $u : T^2 \times [0, T] \rightarrow b\mathbb{Z}$ s. t. $\partial\Psi(u, \dot{u}) + DE(t, u) = 0$
- Energy: $E(u, t) = \int_{J_u} K[\![u]\!]^2 d\mathcal{H}^1 - \bar{\tau}(t) \int_{\Omega} u d\mathcal{H}^2$
- Dissipation: $\Psi(u, \dot{u}) = \int_L \tau_c |v| d\mathcal{H}^1 + \sum_{\text{obstacles}} f_c |v|$



Energy-dissipation functionals

- Space of trajectories: $\mathbb{X} = \{u : [0, T] \rightarrow X\}$,
- Energy-dissipation functional $F_\epsilon : \mathbb{X} \rightarrow \bar{\mathbb{R}}$:

$$F_\epsilon(u) = \int_0^T e^{-t/\epsilon} [\Psi(u, \dot{u}) + \frac{1}{\epsilon} E(t, u)] dt + [e^{-t/\epsilon} E]_0^T$$

↑ ↑ ↑
Dissipation Energy

“Arrow of time”

- Minimum principle: $u \in \operatorname{argmin} F_\epsilon$
- Euler-Lagrange equations (elliptic regularization!):

$$\underline{-\epsilon \partial^2 \Psi(\dot{u}) \ddot{u} + \partial \Psi(\dot{u}) + DE(t, u)} = 0$$



Rate-independent problems

- Energy-dissipation function:

$$F_\epsilon(u) = \int_0^T e^{-t/\epsilon} [\Psi(u, \dot{u}) + \frac{1}{\epsilon} E(t, u)] dt + [e^{-t/\epsilon} E]_0^T$$

- Suppose: i) $\Psi(u, \lambda \dot{u}) = \lambda \Psi(u, \dot{u}), \forall \lambda \geq 0$; ii) There exists $\mathbb{K} \subset \mathbb{X}$ and a functional $J : \mathbb{X} \rightarrow \bar{\mathbb{R}}$ s.t.

$$\Psi(u(t), \dot{u}(t)) = \frac{d}{dt} J(u(t)), \quad \forall u \in \mathbb{K}$$

- Then (deformation theory):

$$F_\epsilon(u) = \begin{cases} \int_0^T e^{-t/\epsilon} [J(u) + E(t, u)] \frac{dt}{\epsilon} + BC, & \text{if } u \in \mathbb{K}, \\ +\infty, & \text{otherwise.} \end{cases}$$

- Pointwise: $u(t) \in \operatorname{argmin}(J(\cdot) + E(t, \cdot))$, provided $u \in \mathbb{K}$



Forest Hardening – Deformation theory

- Monotonicity:

$$\mathbb{K} = \{u \in \mathbb{X}, \text{ s. t. } u(x, t) \geq 0 \text{ and } u(x, t_2) \geq u(x, t_1), t_2 \geq t_1\}$$

- For $u \in \mathbb{K}$ we have $\Psi(u(t), \dot{u}(t)) = \frac{d}{dt}J(u(t))$ with

$$J(u) = \int_{\Omega} \tau_c u d\mathcal{H}^2 + \sum_{\text{obstacles}} f_c u$$

- Deformation-theory minimum principle: Minimize

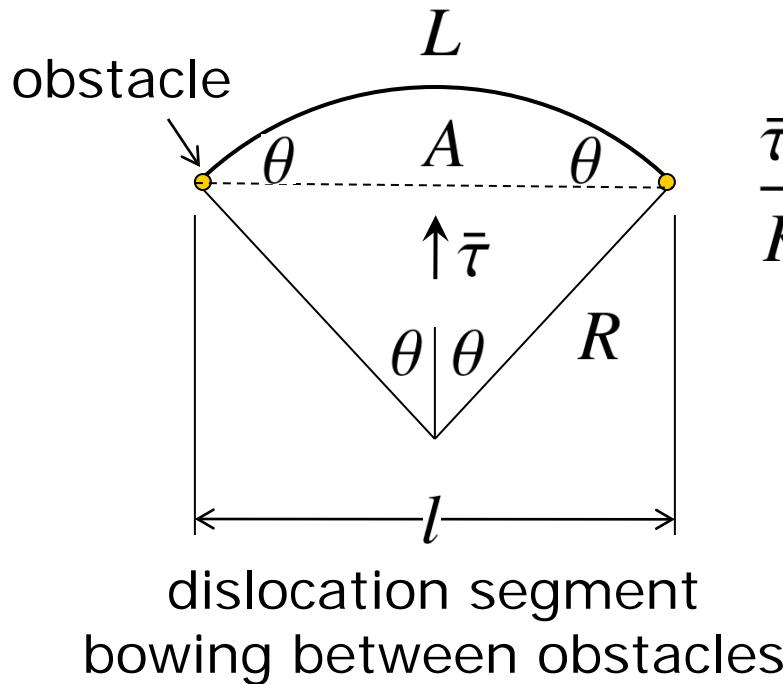
$$J(u) + E(u, t) = \int_{J_u} K[\![u]\!]^2 d\mathcal{H}^1 - \underbrace{(\bar{\tau}(t) - \tau_c)}_{\text{overstress!}} \int_{\Omega} u d\mathcal{H}^2 + \sum_{\text{obstacles}} f_c u$$

- Minimize pseudo-energy $F = J + E$ pointwise in time!



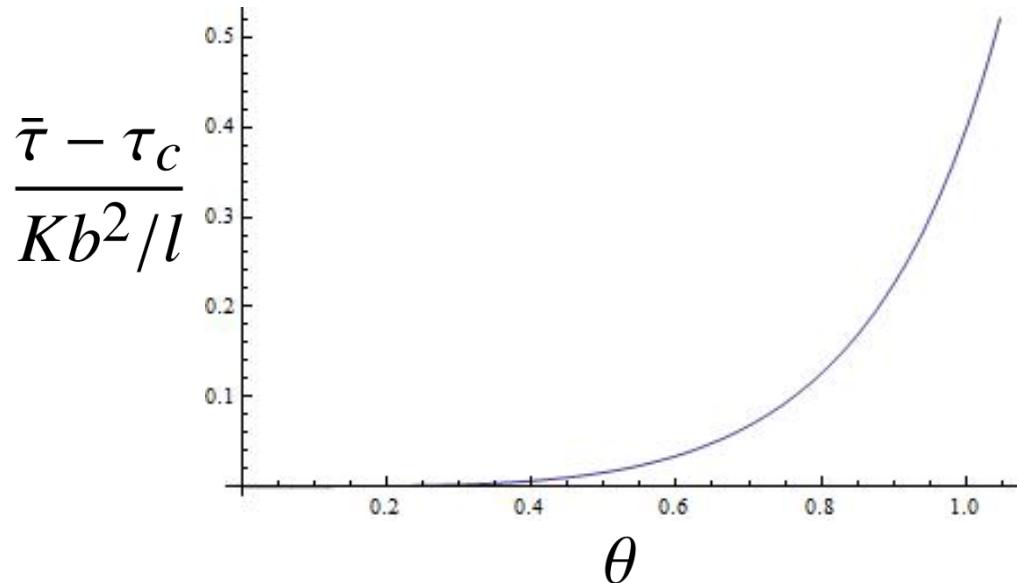
Forest hardening – Pinning/depinning

- Dislocations move by pinning-depinning at obstacles!



- Deformation-theory energy:

$$F(\theta) = Kb^2 L + (\bar{\tau} - \tau_c)A$$

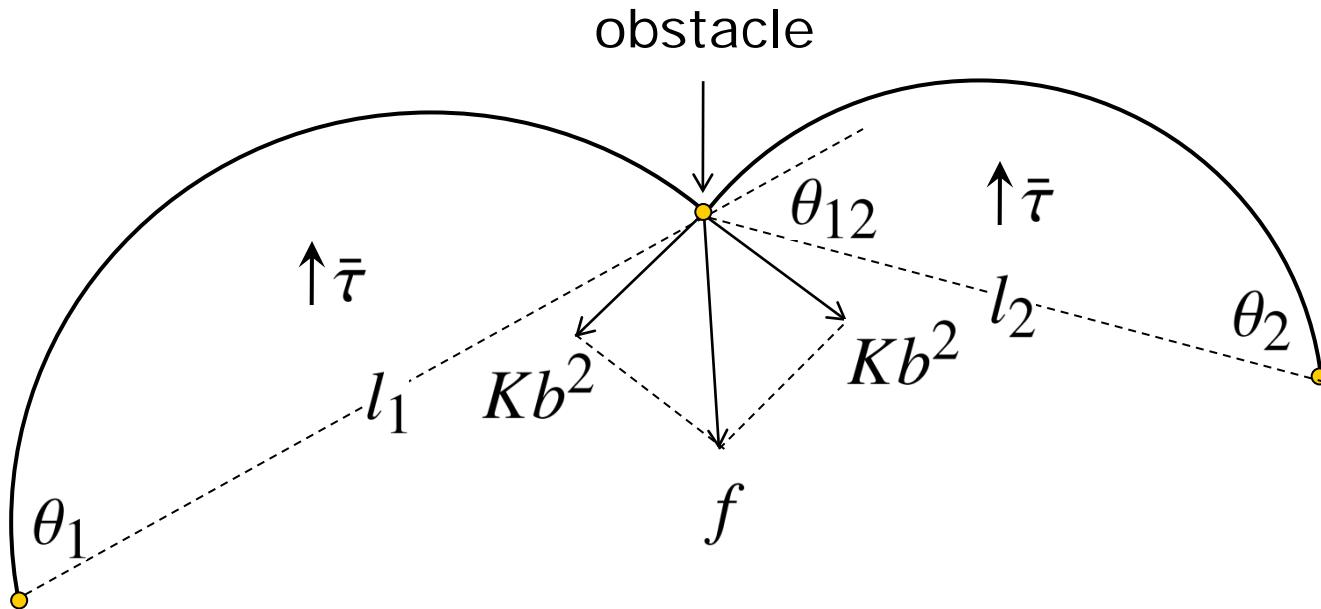


- Equilibrium shape:

$$\frac{dF(\theta)}{d\theta} = 0 \Rightarrow \theta(\bar{\tau}, l)$$



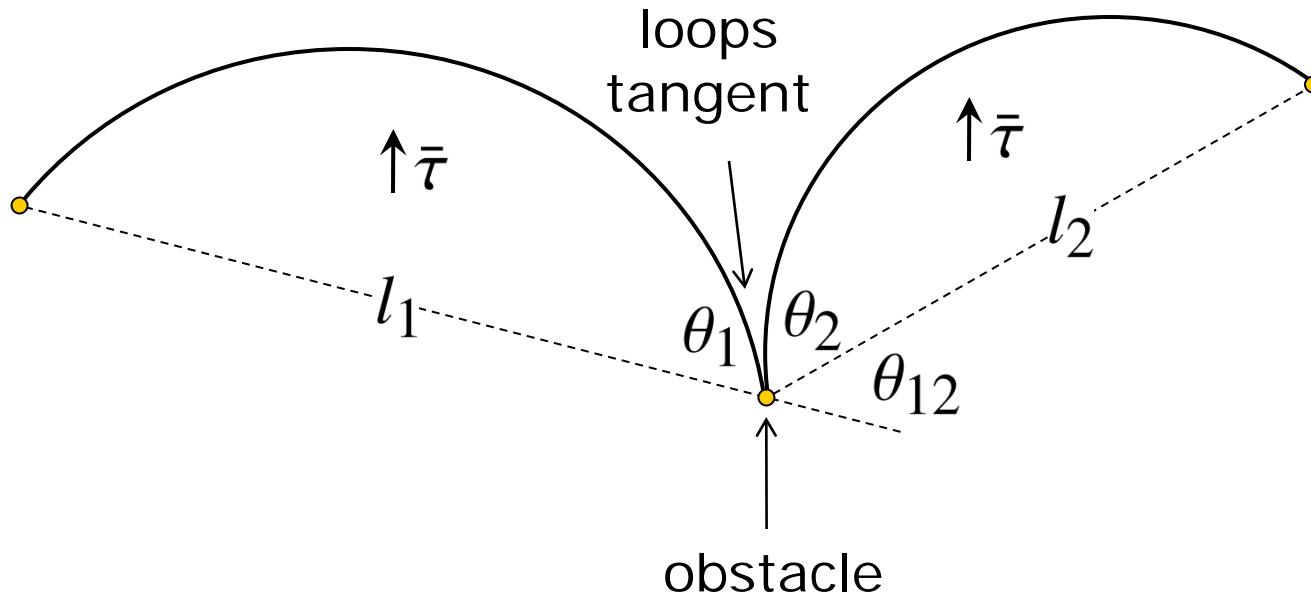
Forest hardening – Pinning/depinning



- Obstacle is stable if: $|f(\bar{\tau}, l_1, l_2, \theta_{12})| < f_c$.
- Otherwise, dislocation depins and moves forward.
- Eventually, dislocation gets pinned down and arrests



Forest hardening – Pinning/depinning

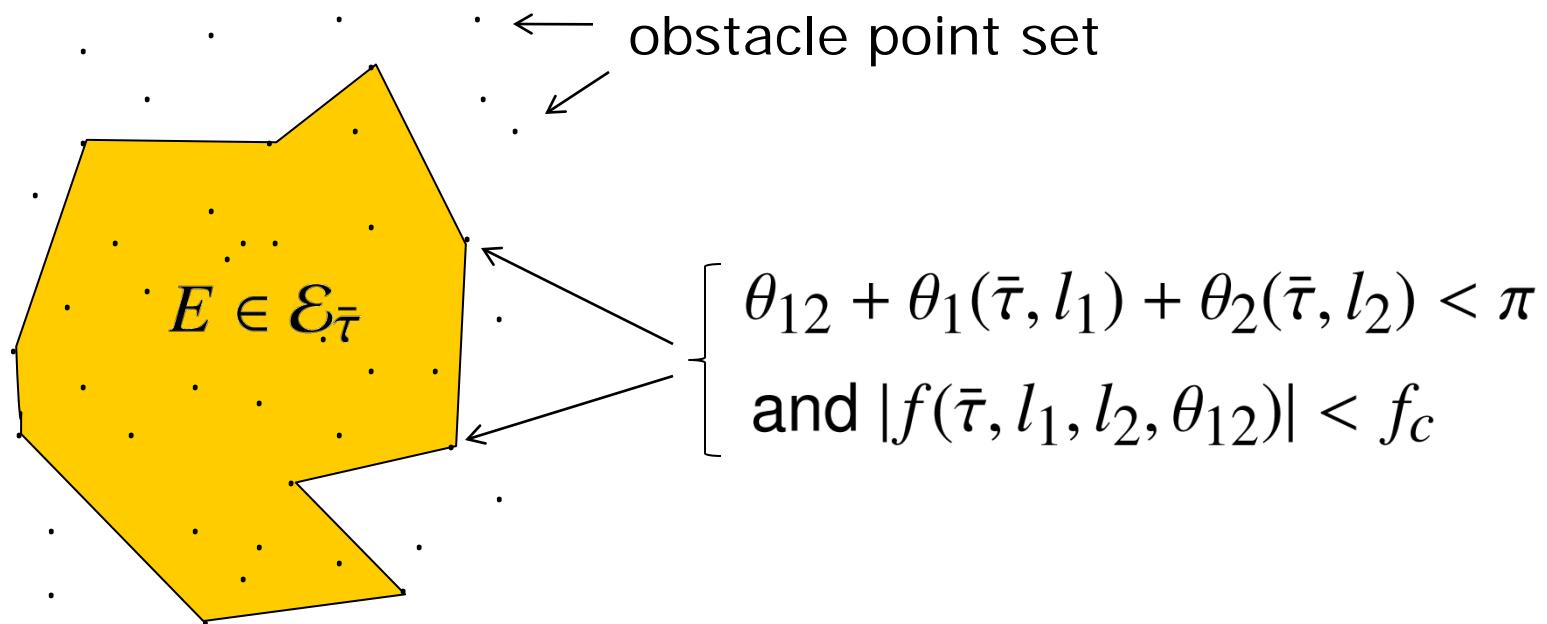


- Obstacle is stable if $\theta_{12} + \theta_1(\bar{\tau}, l_1) + \theta_2(\bar{\tau}, l_2) < \pi$.
- Otherwise, dislocation depins and moves forward.
- Eventually, dislocation gets pinned down and arrests



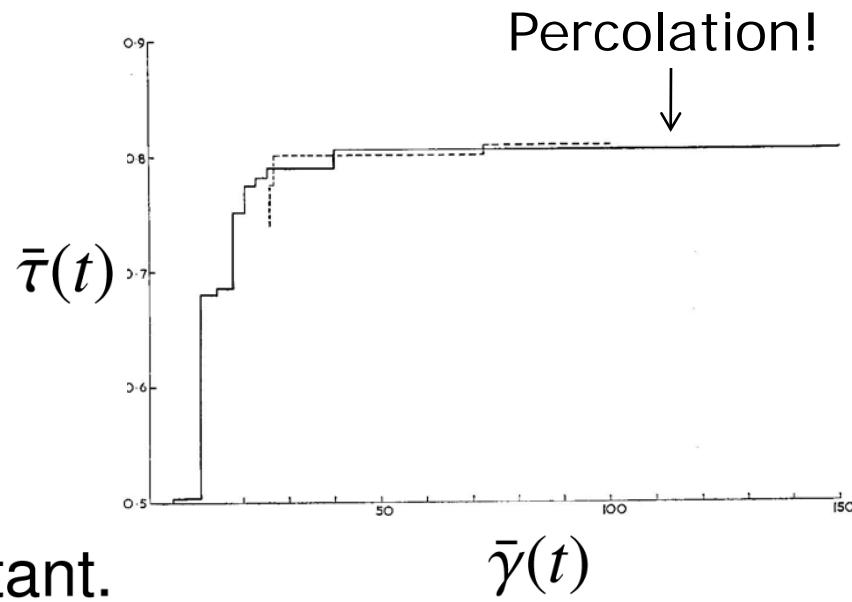
Forest hardening – Single dislocation

- Let \mathcal{E}_s be the set of polygonal domains spanning the obstacle point set such that all vertices are stable for all $\bar{\tau} \leq s$.

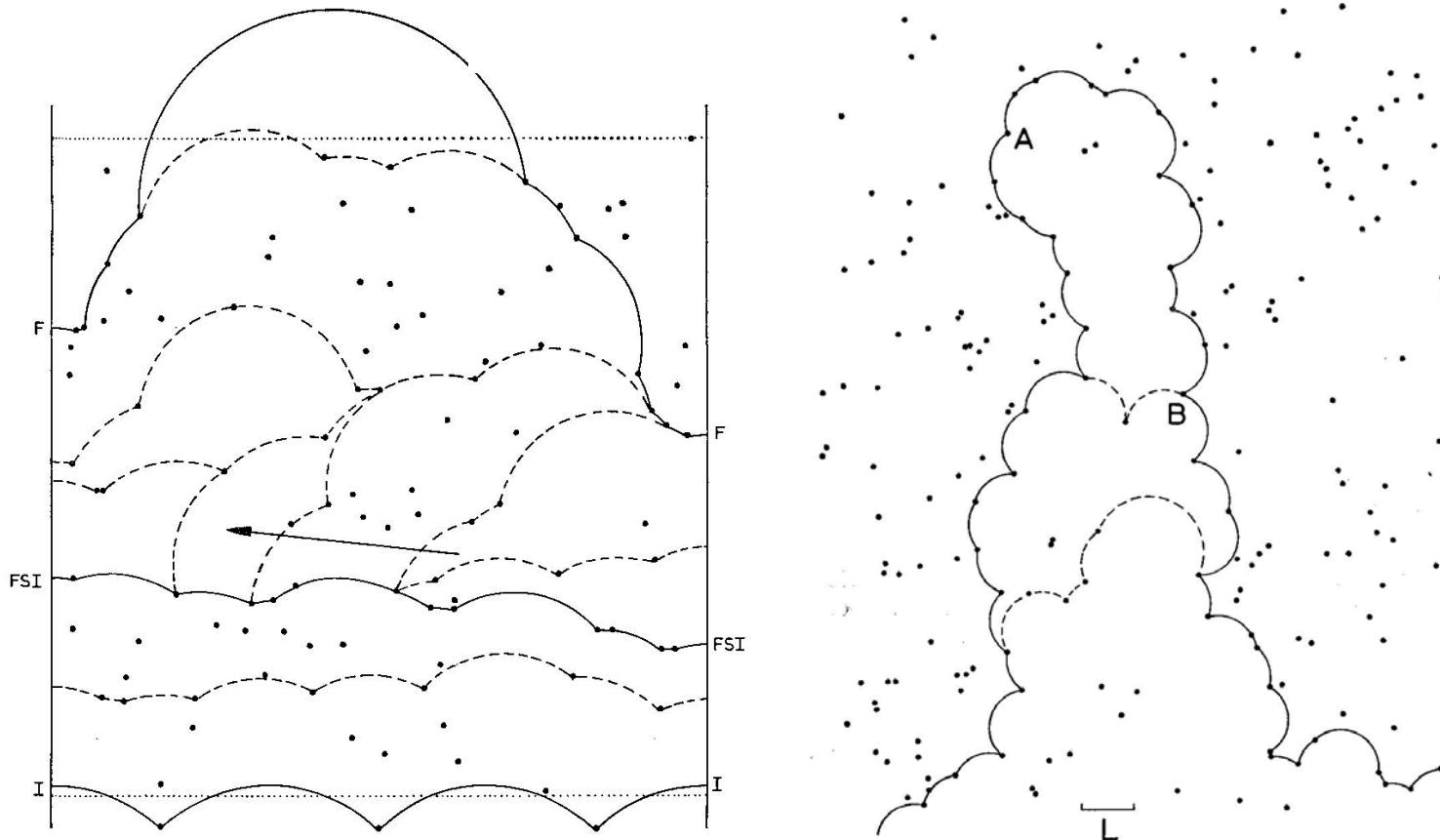


Forest hardening – Single dislocation

- Suppose that $\bar{\tau}(t)$ is increasing, piecewise constant and jumps at times $t_0, t_1, \dots, t_i, \dots$
- Consider a single moving dislocation, $\text{range}(u) = \{0, b\}$.
- Let $u(t_i^-) \rightarrow E(t_i^-) \in \mathcal{E}_{\bar{\tau}(t_i^-)}$.
- Then, $u(t_i^+) \rightarrow E(t_i^+)$ is the smallest set in $\mathcal{E}_{\bar{\tau}(t_i^+)}$ that contains $E(t_i^-)$.
- Slip strain: $\bar{\gamma}(t) = \frac{b|E(t)|}{|\Omega|d}$ increasing, piecewise constant.



Forest hardening – Single dislocation



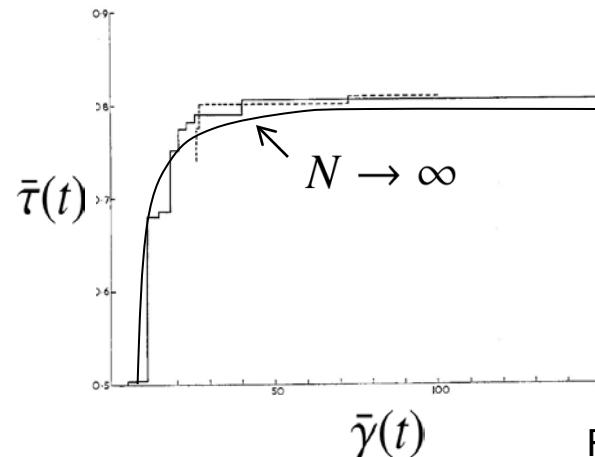
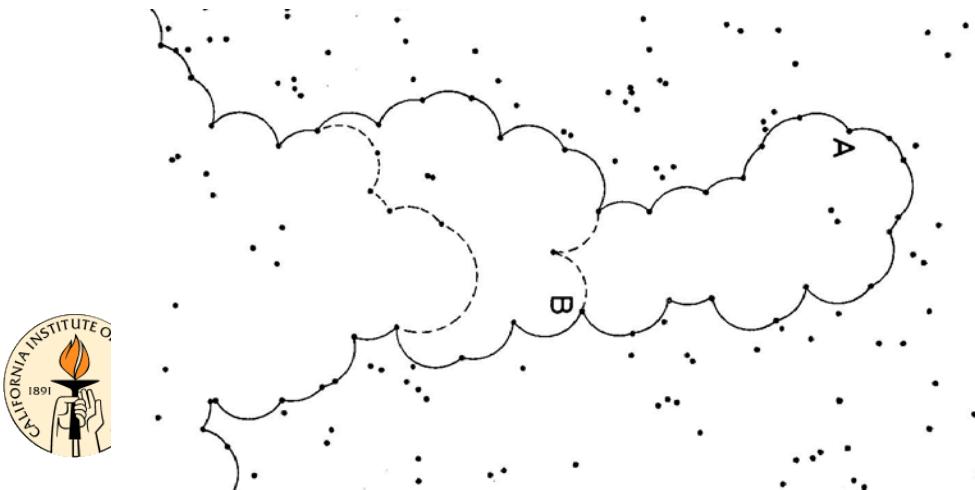
Dislocation motion through random array of obstacles
(Foreman, A.J.E., Makin, M.J., *Phil. Mag.*, **14** (1966) 911)

- Plastic work: $W^p \sim c^{1/2} \bar{\gamma}^{3/2}$, where:
 $c \equiv$ obstacle density, $\bar{\gamma} \equiv$ slip strain

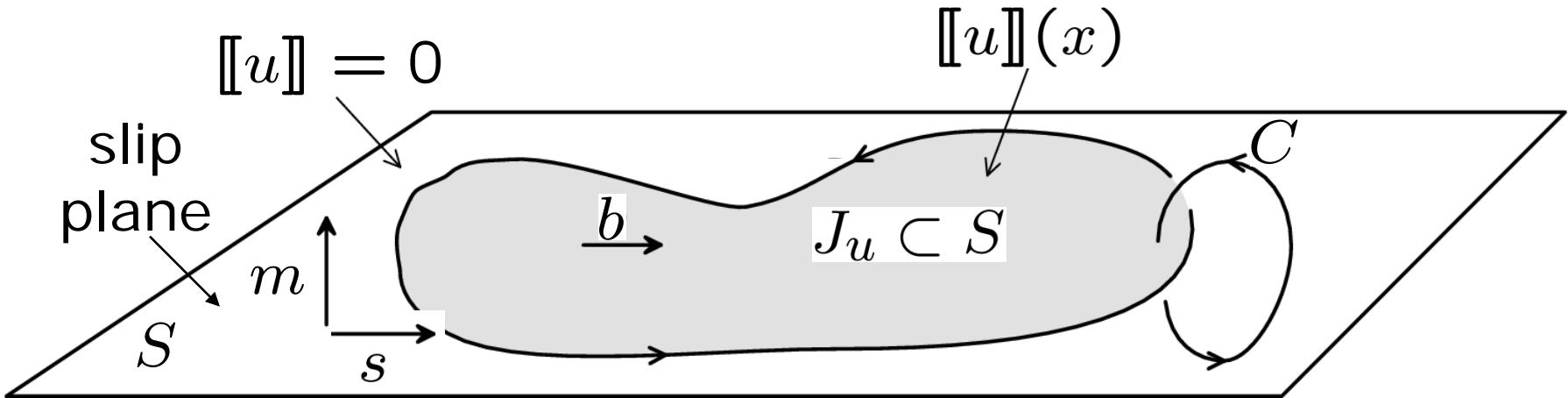


Forest hardening – Summary & outlook

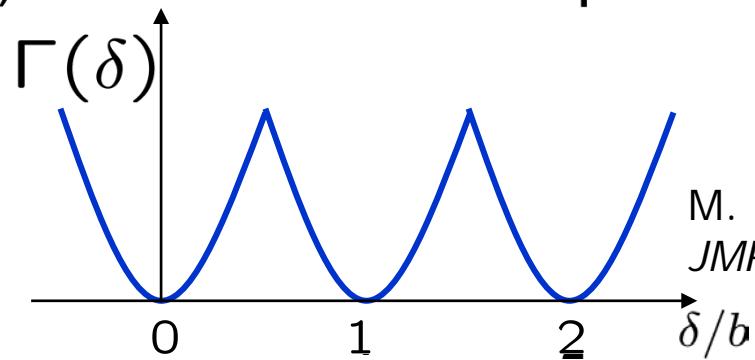
- Model is based on line tension approximation
- Motion by pinning/depinning at obstacles
- Model gives parabolic hardening curve, correct Taylor scaling with obstacle density
- Open mathematical questions:
 - *Limit of infinite number of obstacles (N) at fixed obstacle density, e.g., Poisson distribution of obstacles*
 - *Loading/unloading, hysteresis...*



2½D phase-field model – Assumptions



- i) Activity on single slip system, single slip plane.
- ii) Linear elasticity outside slip plane.
- iii) No Peierls potential (translation invariance).
- iv) Constrained interplanar potential: With $\llbracket u \rrbracket \equiv \delta_s$,



$$\Gamma(\delta) = \frac{\mu}{2d} \text{dist}^2(\delta, b\mathbb{Z})$$

M. Koslowski, A.M.Cuitino and M. Ortiz,
JMPS, **50** (2002) 2597-2635

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2½D phase-field model – Energy

- Total energy: With $u \equiv \delta/b$, $E(u) =$

$$\underbrace{\int_{\mathbb{R}^2} \frac{\mu b^2}{2d} \text{dist}^2(u, \mathbb{Z}) dx}_{\text{Core energy}} + \underbrace{\frac{1}{(2\pi)^2} \int_{\mathbb{R}^2} \frac{\mu b^2}{4} K |\hat{u}|^2 dk}_{\text{Elastic energy}} - \underbrace{\int_{\mathbb{R}^2} b \tau u dx}_{\text{External}}$$

where $K = \frac{k_2^2}{\sqrt{k_1^2 + k_2^2}} + \frac{1}{1 - \nu} \frac{k_1^2}{\sqrt{k_1^2 + k_2^2}}$

- Structure of the energy:

$$E_\epsilon(u) = \frac{1}{2\epsilon} \int_{\mathbb{R}^2} \text{dist}^2(u, \mathbb{Z}) dx + |u|_{H^{1/2}}^2 + \text{linear term}$$

- G. Alberti, G. Bouchitté, and P. Seppecher,
C. R. Acad. Sci. Paris Sér I. Math., **319** (1994) 333–338
- A. Garroni and S. Müller, *SIAM J. Math. Anal.*,
36 (2005) 1943–1964; *ARMA* **181** (2006) 535–578

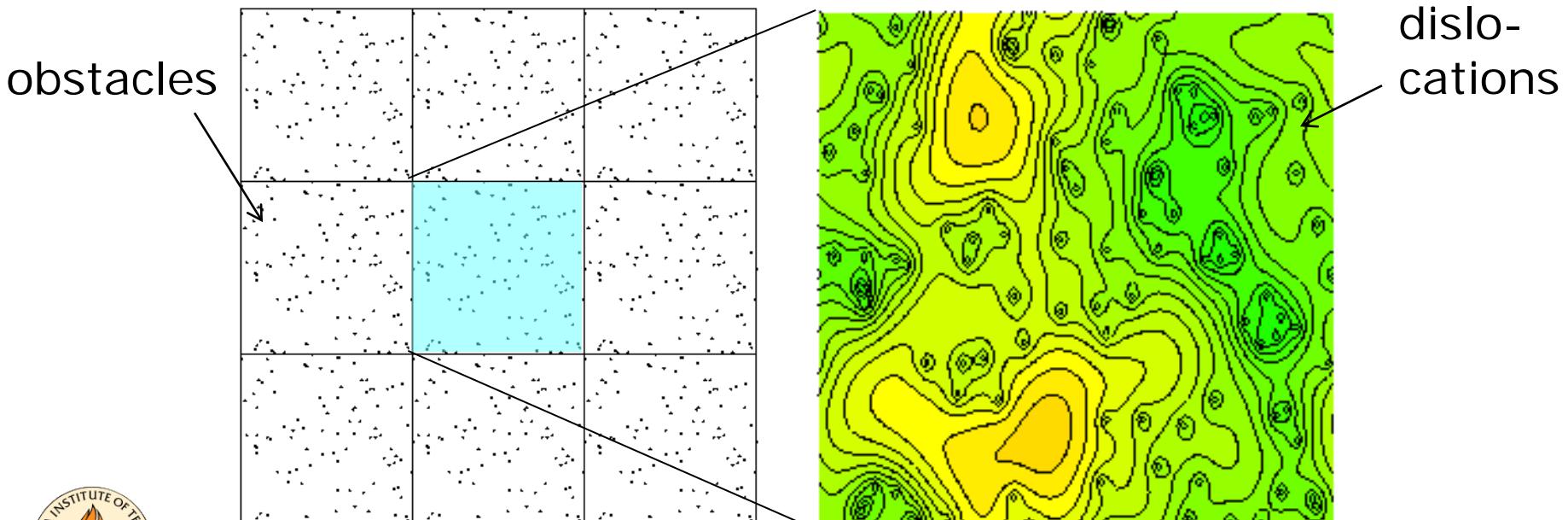


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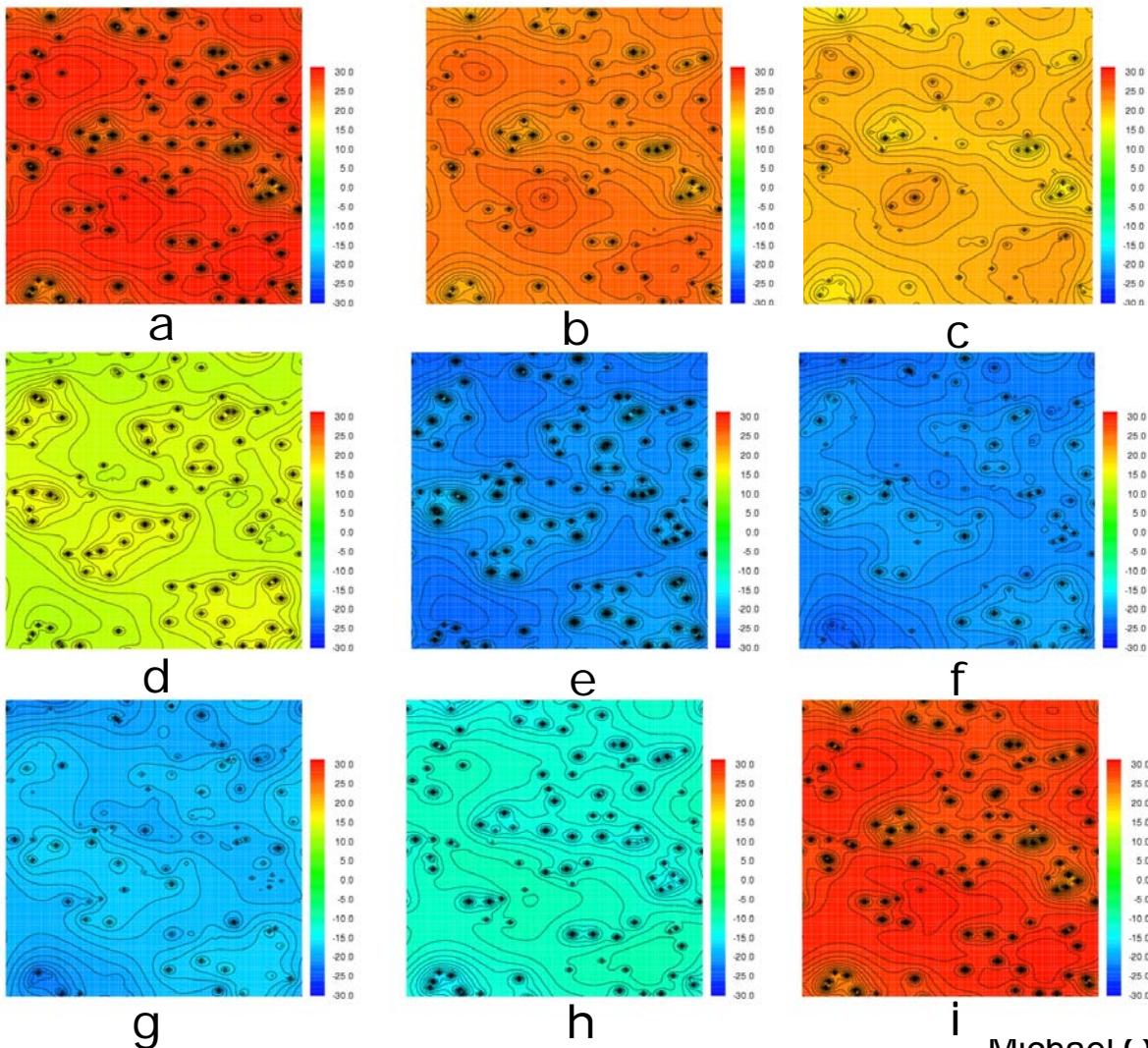
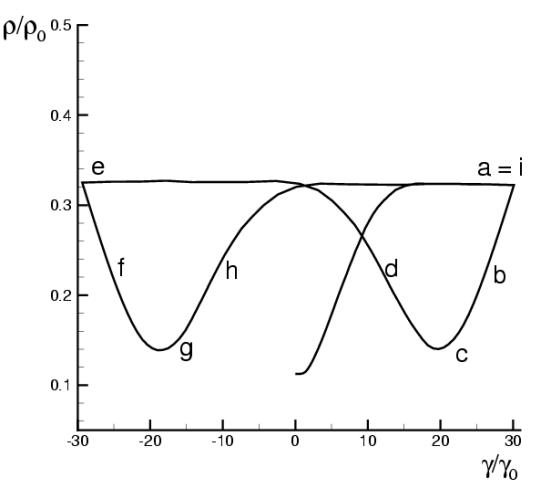
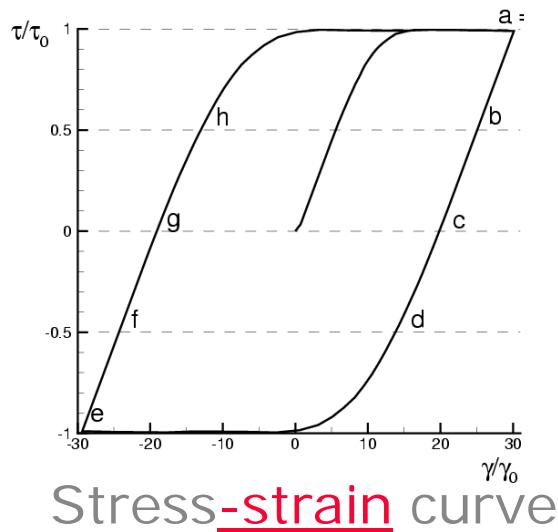
2½D phase-field model – Time discretization

- Time-continuous problem: $\partial\Psi(\dot{u}(t)) + DE(t, u(t)) = 0$
- Time-discrete problem:

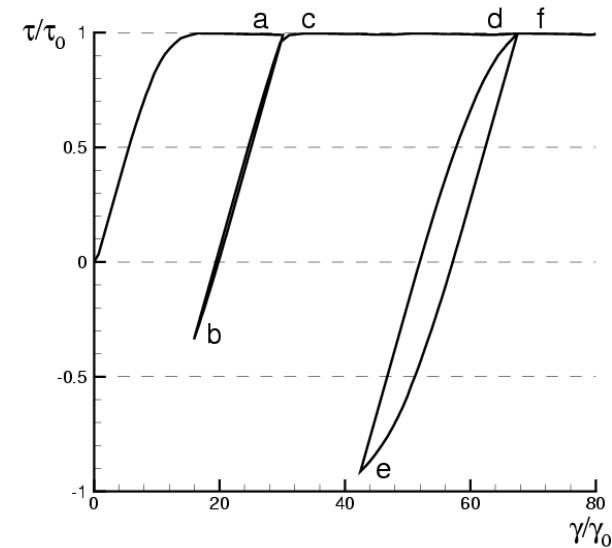
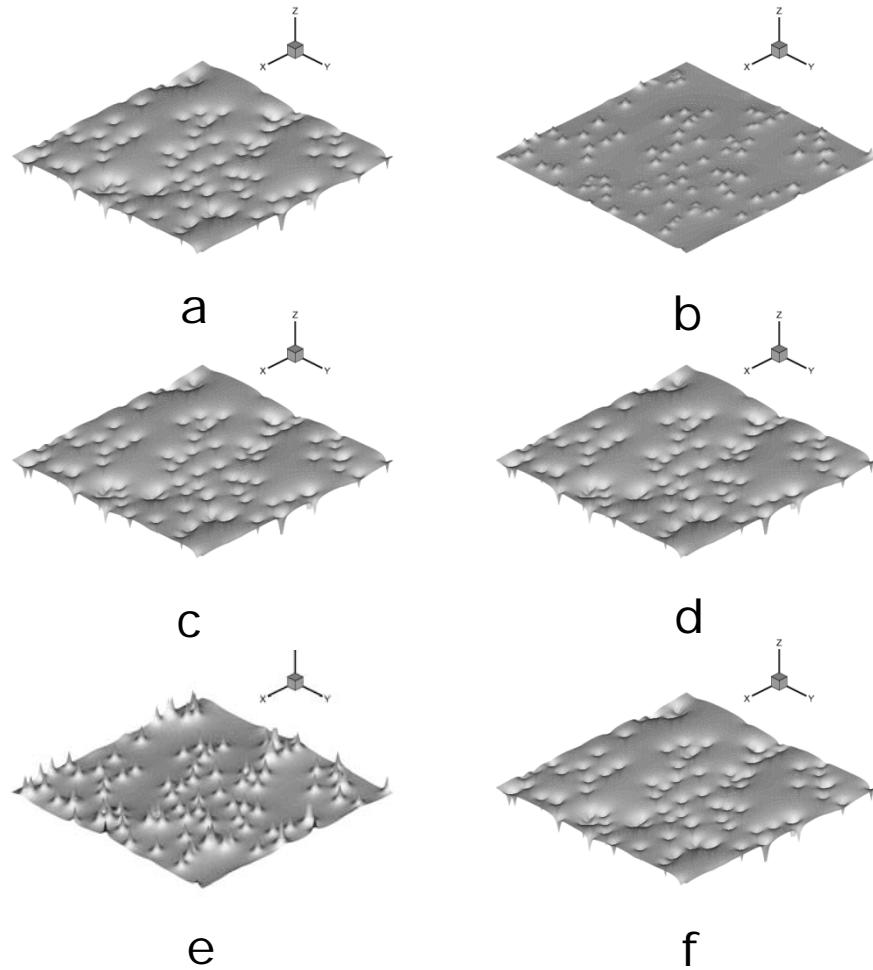
$$E(u_{n+1}) - E(u_n) + \Delta t \Psi\left(\frac{u_{n+1} - u_n}{\Delta t}\right) \rightarrow \text{inf!}$$



Phase-field dislocation dynamics



Return-point and fading memory

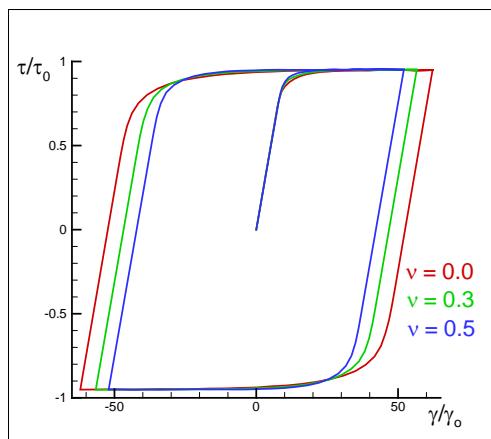


Stress-strain curve.

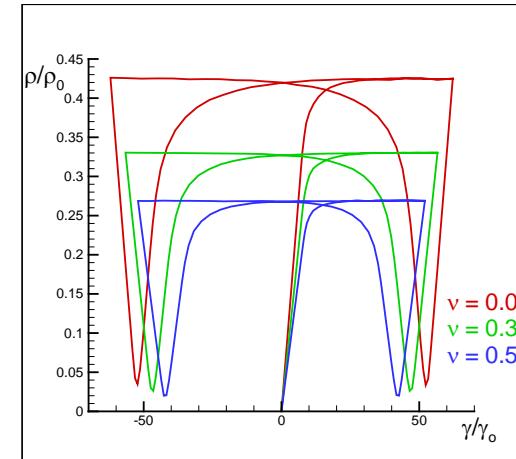
Three dimensional view of the evolution
of the slip-field, showing the the
switching of the cusps.



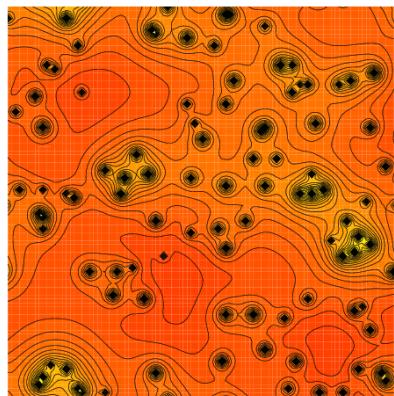
Line-tension anisotropy



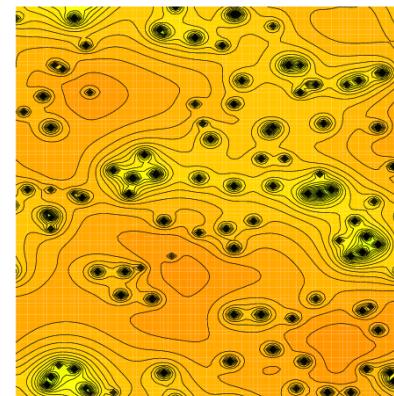
Stress-strain curve.



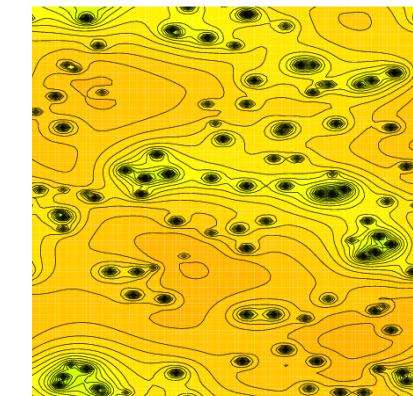
Dislocation density



$\nu = 0.0$



$\nu = 0.3$



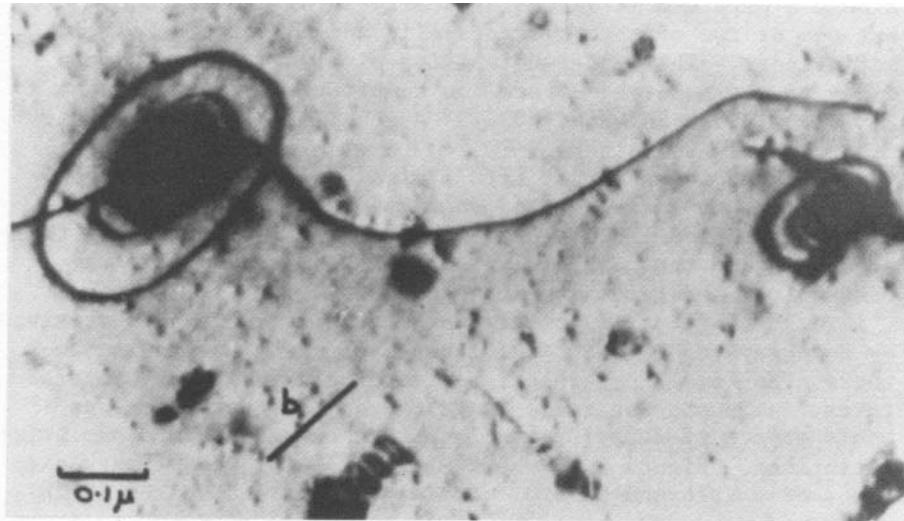
$\nu = 0.5$

b



Summary and outlook

- The forest-hardening model predicts the observed kinetics of hardening in crystals
- A full analytical treatment of the forest-hardening model is still lacking
- Need tools of analysis (similar to CoV) for time dependent evolution problems



(Humphreys and Hirsch, 1970)



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Metal plasticity – Multiscale analysis

